

Table 10-18. Drag of Two-Dimensional Bluff Sections.

Notation C_D = drag coefficient = drag per unit span/($0.5 \rho U^2 D$); D = characteristic width; Drag = force exerted parallel to the approach flow; Re = Reynolds number = UD/ν ; U = free stream velocity; ρ = fluid density; ν = fluid kinematic viscosity. Consistent sets of units are given in Table 3-1. Data are for high Reynolds number, $Re > \sim 10^4$, incompressible, low-turbulent flow. \rightarrow denotes direction of approaching free stream unless otherwise noted. Accuracy is approximately $\pm 5\%$.



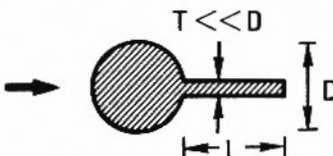
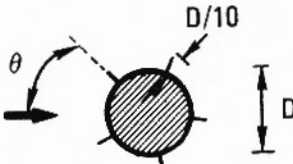
Geometry	Drag Coefficient, C_D , and Remarks																																							
1. Circular Cylinder 	<table><tr><th>Re</th><th>10^2</th><th>10^3</th><th>10^4</th><th>10^5</th><th>10^6</th><th>10^7</th></tr><tr><th>C_D</th><td>1.4</td><td>1.0</td><td>1.1</td><td>1.2</td><td>0.4</td><td>0.8</td></tr></table> <p>For $Re < 1$, $C_D \approx 8\pi/[Re \log_e (7.4/Re)]$. Also see Fig. 10-22. Ref. 10-134</p>	Re	10^2	10^3	10^4	10^5	10^6	10^7	C_D	1.4	1.0	1.1	1.2	0.4	0.8																									
Re	10^2	10^3	10^4	10^5	10^6	10^7																																		
C_D	1.4	1.0	1.1	1.2	0.4	0.8																																		
2. Stranded Cable or Chain 	<table><tr><th>Type</th><th>$10^3 < Re < 10^4$</th><th>$10^4 < Re < 10^5$</th></tr><tr><td>Stranded Steel Cable</td><td>1.5</td><td>1.3</td></tr><tr><td>Jacked Steel Cable</td><td>1.5</td><td>1.1</td></tr><tr><td>Braided Synthetic Cable</td><td>1.1</td><td>1.1</td></tr><tr><td>Plaited Synthetic Cable</td><td>1.2</td><td>0.99</td></tr><tr><td>Link Chain (Based on Link Width)</td><td>--</td><td>0.85</td></tr></table>		Type	$10^3 < Re < 10^4$	$10^4 < Re < 10^5$	Stranded Steel Cable	1.5	1.3	Jacked Steel Cable	1.5	1.1	Braided Synthetic Cable	1.1	1.1	Plaited Synthetic Cable	1.2	0.99	Link Chain (Based on Link Width)	--	0.85	Ref. 10-159.																			
Type	$10^3 < Re < 10^4$	$10^4 < Re < 10^5$																																						
Stranded Steel Cable	1.5	1.3																																						
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Link Chain (Based on Link Width)	--	0.85																																						
3. Circular Cylinder with Thin Fin 	<table><tr><th>L/D</th><th>0</th><th>0.33</th><th>0.67</th><th>1.0</th><th>1.5</th><th>2.0</th><th>2.5</th></tr><tr><th>C_D</th><td>1.25</td><td>1.2</td><td>1.15</td><td>1.1</td><td>1.07</td><td>1.02</td><td>1.0</td></tr></table> <p>$Re = 10^5$, Ref. 10-160</p>	L/D	0	0.33	0.67	1.0	1.5	2.0	2.5	C_D	1.25	1.2	1.15	1.1	1.07	1.02	1.0																							
L/D	0	0.33	0.67	1.0	1.5	2.0	2.5																																	
C_D	1.25	1.2	1.15	1.1	1.07	1.02	1.0																																	
4. Cylinder with Five Thin Fins 	<table><tr><th>θ</th><th>C_D</th><th>C_L</th></tr><tr><td>-20</td><td>2.2</td><td>0.3</td></tr><tr><td>-10</td><td>2.5</td><td>0.25</td></tr><tr><td>0</td><td>2.7</td><td>0.0</td></tr><tr><td>10</td><td>2.5</td><td>-0.25</td></tr><tr><td>20</td><td>2.1</td><td>-0.4</td></tr><tr><td>30</td><td>1.5</td><td>-0.25</td></tr><tr><td>35</td><td>1.1</td><td>0.0</td></tr><tr><td>40</td><td>1.4</td><td>0.2</td></tr><tr><td>50</td><td>2.0</td><td>0.4</td></tr><tr><td>60</td><td>2.4</td><td>0.35</td></tr></table> <p>$Re = 10^4$, Ref. 10-161.</p>	θ	C_D	C_L	-20	2.2	0.3	-10	2.5	0.25	0	2.7	0.0	10	2.5	-0.25	20	2.1	-0.4	30	1.5	-0.25	35	1.1	0.0	40	1.4	0.2	50	2.0	0.4	60	2.4	0.35						
θ	C_D	C_L																																						
-20	2.2	0.3																																						
-10	2.5	0.25																																						
0	2.7	0.0																																						
10	2.5	-0.25																																						
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Table 10-18. Drag of Two-Dimensional Bluff Sections. (Continued)

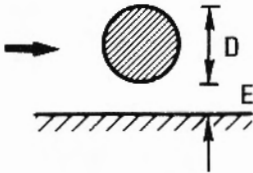
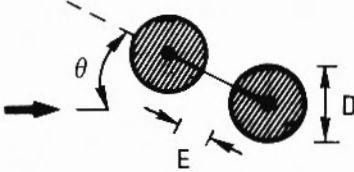
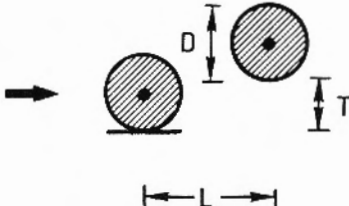
Geometry	Drag Coefficient, C_D , and Remarks																																																						
5. Cylinder Near a Wall																																																							
	<table><tr><th>E/D</th><th>C_D</th><th>C_L</th></tr><tr><td>0</td><td>0.8</td><td>0.6</td></tr><tr><td>0.25</td><td>1.1</td><td>0.25</td></tr><tr><td>0.5</td><td>1.2</td><td>0.15</td></tr><tr><td>1.0</td><td>1.3</td><td>0.05</td></tr><tr><td>1.5</td><td>1.2</td><td>0.02</td></tr><tr><td>2.0</td><td>1.2</td><td>0</td></tr><tr><td>4.0</td><td>1.2</td><td>0</td></tr><tr><td>6.0</td><td>1.2</td><td>0</td></tr></table>	E/D	C_D	C_L	0	0.8	0.6	0.25	1.1	0.25	0.5	1.2	0.15	1.0	1.3	0.05	1.5	1.2	0.02	2.0	1.2	0	4.0	1.2	0	6.0	1.2	0																											
E/D	C_D	C_L																																																					
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4.0	1.2	0																																																					
6.0	1.2	0																																																					
	Re = 2×10^4 , Ref. 10-162 Lift force is away from wall.																																																						
6. Two Cylinders in Tandem																																																							
	<table><tr><th rowspan="3">θ (deg)</th><th colspan="5">C_D</th></tr><tr><th colspan="5">E/D</th></tr><tr><th>0.625</th><th>1.0</th><th>2.0</th><th>3.0</th><th>∞</th></tr><tr><td>0</td><td>0.3</td><td>0.3</td><td>0.3</td><td>0.3</td><td>2.4</td></tr><tr><td>10</td><td>0.4</td><td>0.4</td><td>0.45</td><td>0.4</td><td>2.4</td></tr><tr><td>20</td><td>0.7</td><td>0.7</td><td>0.6</td><td>0.5</td><td>2.4</td></tr><tr><td>30</td><td>0.8</td><td>0.8</td><td>0.6</td><td>0.5</td><td>2.4</td></tr><tr><td>40</td><td>0.9</td><td>0.85</td><td>0.6</td><td>0.5</td><td>2.4</td></tr><tr><td>50</td><td>1.0</td><td>0.9</td><td>0.7</td><td>0.55</td><td>2.4</td></tr></table>			θ (deg)	C_D					E/D					0.625	1.0	2.0	3.0	∞	0	0.3	0.3	0.3	0.3	2.4	10	0.4	0.4	0.45	0.4	2.4	20	0.7	0.7	0.6	0.5	2.4	30	0.8	0.8	0.6	0.5	2.4	40	0.9	0.85	0.6	0.5	2.4	50	1.0	0.9	0.7	0.55	2.4
θ (deg)	C_D																																																						
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50	1.0	0.9	0.7	0.55	2.4																																																		
	Ref. 10-163																																																						
7. Cylinder Downstream of Another Cylinder																																																							
	<table><tr><th colspan="2">T/D = 0</th><th colspan="2">T/D = 0.5</th></tr><tr><th>L/D</th><th>C_D</th><th>L/D</th><th>C_D</th></tr><tr><td>1.0</td><td>-0.4</td><td>1.0</td><td>0.65</td></tr><tr><td>1.5</td><td>-0.2</td><td>1.5</td><td>0.50</td></tr><tr><td>2.0</td><td>0.0</td><td>2.0</td><td>0.45</td></tr><tr><td>2.5</td><td>0.2</td><td>2.5</td><td>0.45</td></tr><tr><td>3.0</td><td>0.2</td><td>3.0</td><td>0.40</td></tr><tr><td>4.0</td><td>0.3</td><td>4.0</td><td>0.40</td></tr></table>			T/D = 0		T/D = 0.5		L/D	C_D	L/D	C_D	1.0	-0.4	1.0	0.65	1.5	-0.2	1.5	0.50	2.0	0.0	2.0	0.45	2.5	0.2	2.5	0.45	3.0	0.2	3.0	0.40	4.0	0.3	4.0	0.40																				
T/D = 0		T/D = 0.5																																																					
L/D	C_D	L/D	C_D																																																				
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Drag on Downstream Cylinder.	<table><tr><th colspan="2">T/D = 1.0</th><th colspan="2">T/D = 2</th></tr><tr><th>L/D</th><th>C_D</th><th>L/D</th><th>C_D</th></tr><tr><td>1.0</td><td>1.1</td><td>1.0</td><td>1.1</td></tr><tr><td>1.5</td><td>1.0</td><td>1.5</td><td>1.0</td></tr><tr><td>2.0</td><td>0.70</td><td>2.0</td><td>1.0</td></tr><tr><td>2.5</td><td>0.70</td><td>2.5</td><td>1.0</td></tr><tr><td>3.0</td><td>0.65</td><td>3.0</td><td>1.0</td></tr><tr><td>4.0</td><td>0.65</td><td>4.0</td><td>1.0</td></tr></table>			T/D = 1.0		T/D = 2		L/D	C_D	L/D	C_D	1.0	1.1	1.0	1.1	1.5	1.0	1.5	1.0	2.0	0.70	2.0	1.0	2.5	0.70	2.5	1.0	3.0	0.65	3.0	1.0	4.0	0.65	4.0	1.0																				
T/D = 1.0		T/D = 2																																																					
L/D	C_D	L/D	C_D																																																				
1.0	1.1	1.0	1.1																																																				
1.5	1.0	1.5	1.0																																																				
2.0	0.70	2.0	1.0																																																				
2.5	0.70	2.5	1.0																																																				
3.0	0.65	3.0	1.0																																																				
4.0	0.65	4.0	1.0																																																				
	$10^4 < Re < 10^5$, Ref. 10-164																																																						

Table 10-18. Drag of Two-Dimensional Bluff Sections. (Continued)

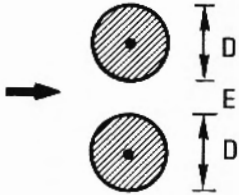
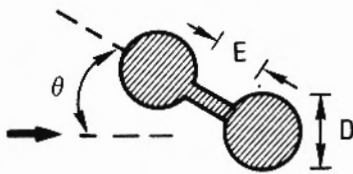
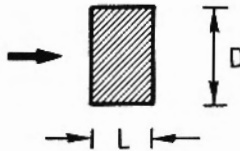
Geometry	Drag Coefficient, C_D , and Remarks																																				
8. Two Cylinders Side by Side																																					
	<table><tr><th>E/D</th><th>C_D</th><th>C_L</th></tr><tr><td>0</td><td>1.6</td><td>0.8</td></tr><tr><td>0.25</td><td>1.0</td><td>0.6</td></tr><tr><td>0.5</td><td>0.9</td><td>0.4</td></tr><tr><td>1.0</td><td>1.1</td><td>0.2</td></tr><tr><td>1.5</td><td>1.3</td><td>0.1</td></tr><tr><td>2.0</td><td>1.2</td><td>0.05</td></tr><tr><td>4.0</td><td>1.2</td><td>0.0</td></tr><tr><td>6.0</td><td>1.2</td><td>0.0</td></tr></table>	E/D	C_D	C_L	0	1.6	0.8	0.25	1.0	0.6	0.5	0.9	0.4	1.0	1.1	0.2	1.5	1.3	0.1	2.0	1.2	0.05	4.0	1.2	0.0	6.0	1.2	0.0									
E/D	C_D	C_L																																			
0	1.6	0.8																																			
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2.0	1.2	0.05																																			
4.0	1.2	0.0																																			
6.0	1.2	0.0																																			
	C_D, C_L for each cylinder. $10^4 < Re < 10^5$, Ref. 10-164. Lift force is repulsive.																																				
9. Two Cylinders Connected by a Thin Web																																					
	<table><tr><th rowspan="3">θ (deg)</th><th colspan="3">C_D</th></tr><tr><th colspan="3">E/D</th></tr><tr><th>1.0</th><th>2.0</th><th>3.0</th></tr><tr><td>0</td><td>0.25</td><td>0.3</td><td>0.3</td></tr><tr><td>10</td><td>0.4</td><td>0.4</td><td>0.4</td></tr><tr><td>20</td><td>0.7</td><td>0.7</td><td>0.7</td></tr><tr><td>30</td><td>1.0</td><td>1.0</td><td>1.2</td></tr><tr><td>40</td><td>1.3</td><td>1.4</td><td>1.8</td></tr><tr><td>50</td><td>1.7</td><td>1.8</td><td>2.5</td></tr></table>	θ (deg)	C_D			E/D			1.0	2.0	3.0	0	0.25	0.3	0.3	10	0.4	0.4	0.4	20	0.7	0.7	0.7	30	1.0	1.0	1.2	40	1.3	1.4	1.8	50	1.7	1.8	2.5		
θ (deg)	C_D																																				
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	Ref. 10-163.																																				
10. Rectangle																																					
	<table><tr><th>L/D</th><th>C_D</th><th>L/D</th><th>C_D</th></tr><tr><td>0.1 ≤</td><td>1.9</td><td>1.0</td><td>2.2</td></tr><tr><td>0.2</td><td>2.1</td><td>1.2</td><td>2.1</td></tr><tr><td>0.4</td><td>2.35</td><td>1.5</td><td>1.8</td></tr><tr><td>0.5</td><td>2.5</td><td>2.0</td><td>1.6</td></tr><tr><td>0.65</td><td>2.9</td><td>2.5</td><td>1.4</td></tr><tr><td>0.8</td><td>2.3</td><td>3.0</td><td>1.3</td></tr><tr><td></td><td></td><td>6.0</td><td>0.89</td></tr></table>	L/D	C_D	L/D	C_D	0.1 ≤	1.9	1.0	2.2	0.2	2.1	1.2	2.1	0.4	2.35	1.5	1.8	0.5	2.5	2.0	1.6	0.65	2.9	2.5	1.4	0.8	2.3	3.0	1.3			6.0	0.89				
L/D	C_D	L/D	C_D																																		
0.1 ≤	1.9	1.0	2.2																																		
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	$Re \sim 10^5$, Refs. 10-165; 10-102, p. 10-3.																																				

Table 10-18. Drag of Two-Dimensional Bluff Sections. (Continued)

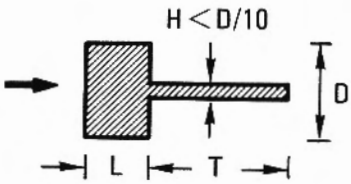
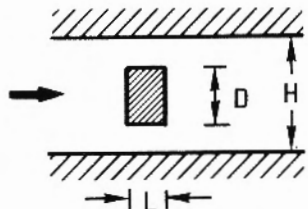
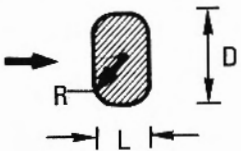
Geometry	Drag Coefficient, C_D , and Remarks																																											
<p>11. Rectangle with Thin Splitter Plate</p> 	<table><tr><th rowspan="3">L/D</th><th colspan="3">C_D</th></tr><tr><th colspan="3">T/D</th></tr><tr><th>0</th><th>5</th><th>10</th></tr><tr><td>0.1 <</td><td>1.9</td><td>1.4</td><td>1.38</td></tr><tr><td>0.2</td><td>2.1</td><td>1.40</td><td>1.43</td></tr><tr><td>0.4</td><td>2.35</td><td>1.39</td><td>1.46</td></tr><tr><td>0.6</td><td>1.8</td><td>1.38</td><td>1.48</td></tr><tr><td>0.8</td><td>2.3</td><td>1.36</td><td>1.47</td></tr><tr><td>1.0</td><td>2.0</td><td>1.33</td><td>1.45</td></tr><tr><td>1.5</td><td>1.8</td><td>1.30</td><td>1.40</td></tr><tr><td>2.0</td><td>1.6</td><td>--</td><td>1.33</td></tr></table> <p>$Re = 5 \times 10^4$, Refs. 10-131, 10-166.</p>	L/D	C_D			T/D			0	5	10	0.1 <	1.9	1.4	1.38	0.2	2.1	1.40	1.43	0.4	2.35	1.39	1.46	0.6	1.8	1.38	1.48	0.8	2.3	1.36	1.47	1.0	2.0	1.33	1.45	1.5	1.8	1.30	1.40	2.0	1.6	--	1.33	
L/D	C_D																																											
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	0	5	10																																									
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0.8	2.3	1.36	1.47																																									
1.0	2.0	1.33	1.45																																									
1.5	1.8	1.30	1.40																																									
2.0	1.6	--	1.33																																									
<p>12. Rectangle in a Channel</p> 	$C_D = \left(1 - \frac{D}{H}\right)^{-n} C_D \Big _{H=\infty}$ <p style="text-align: right;">frame 10</p> <p>for $0 < D/H < 0.25$.</p> <table><tr><td>L/D</td><td>0.1 <</td><td>0.25</td><td>0.50</td><td>1.0</td><td>2.0</td></tr><tr><td>n</td><td>2.3</td><td>2.2</td><td>2.1</td><td>1.2</td><td>0.4</td></tr></table> <p>$Re > 10^3$, Ref. 10-131.</p>	L/D	0.1 <	0.25	0.50	1.0	2.0	n	2.3	2.2	2.1	1.2	0.4																															
L/D	0.1 <	0.25	0.50	1.0	2.0																																							
n	2.3	2.2	2.1	1.2	0.4																																							
<p>13. Rectangle with Rounded Corners</p> 	<table><tr><td>L/D</td><td>R/D</td><td>C_D</td><td>L/D</td><td>R/D</td><td>C_D</td></tr><tr><td rowspan="5">0.5</td><td>0</td><td>2.5</td><td rowspan="5">2.0</td><td>0</td><td>1.6</td></tr><tr><td>0.021</td><td>2.2</td><td>0.042</td><td>1.4</td></tr><tr><td>0.083</td><td>1.9</td><td>0.167</td><td>0.7</td></tr><tr><td rowspan="2">0.250</td><td colspan="2" rowspan="2">1.6</td><td>0.50</td><td>0.4</td></tr><tr><td></td><td></td></tr><tr><td rowspan="5">1.0</td><td>0</td><td>2.2</td><td rowspan="5">6.0</td><td>0.</td><td>0.89</td></tr><tr><td>0.021</td><td>2.0</td><td rowspan="4">0.5</td><td rowspan="4">0.29</td></tr><tr><td>0.167</td><td>1.2</td></tr><tr><td rowspan="2">0.333</td><td colspan="2" rowspan="2">1.0</td></tr><tr><td></td></tr></table> <p>$Re = 10^5$, Refs. 10-132; 10-162; 10-102, p. 10-3.</p>	L/D	R/D	C_D	L/D	R/D	C_D	0.5	0	2.5	2.0	0	1.6	0.021	2.2	0.042	1.4	0.083	1.9	0.167	0.7	0.250	1.6		0.50	0.4			1.0	0	2.2	6.0	0.	0.89	0.021	2.0	0.5	0.29	0.167	1.2	0.333	1.0		
L/D	R/D	C_D	L/D	R/D	C_D																																							
0.5	0	2.5	2.0	0	1.6																																							
	0.021	2.2		0.042	1.4																																							
	0.083	1.9		0.167	0.7																																							
	0.250	1.6		0.50	0.4																																							
1.0	0	2.2	6.0	0.	0.89																																							
	0.021	2.0		0.5	0.29																																							
	0.167	1.2																																										
	0.333	1.0																																										

Table 10-18. Drag of Two-Dimensional Bluff Sections. (Continued)

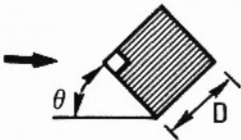
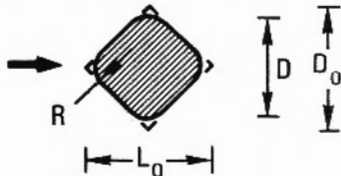
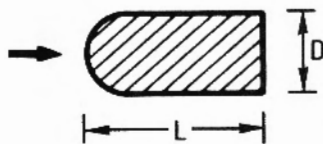
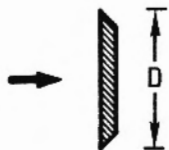
Geometry	Drag Coefficient, C_D , and Remarks																												
14. Inclined Square 	<table><tr><th>θ (Deg)</th><td>0</td><td>5</td><td>10</td><td>15</td><td>20</td><td>25</td><td>30</td><td>35</td><td>40</td><td>45</td></tr><tr><th>C_D</th><td>2.2</td><td>2.1</td><td>1.8</td><td>1.3</td><td>1.9</td><td>2.1</td><td>2.2</td><td>2.3</td><td>2.4</td><td>2.4</td></tr></table> <p>$Re = 4.7 \times 10^4$, Ref. 10-275.</p>	θ (Deg)	0	5	10	15	20	25	30	35	40	45	C_D	2.2	2.1	1.8	1.3	1.9	2.1	2.2	2.3	2.4	2.4						
θ (Deg)	0	5	10	15	20	25	30	35	40	45																			
C_D	2.2	2.1	1.8	1.3	1.9	2.1	2.2	2.3	2.4	2.4																			
15. Diamond with Rounded Corners 	<table><tr><th>L_o/D_o</th><th>R/D_o</th><th>C_D</th><th></th></tr><tr><td rowspan="3">0.5</td><td>0.021</td><td>1.8</td><td rowspan="3">Fore and aft corners not rounded.</td></tr><tr><td>0.083</td><td>1.7</td></tr><tr><td>0.167</td><td>1.7</td></tr><tr><td rowspan="3">1.0</td><td>0.015</td><td>1.5</td><td rowspan="3"></td></tr><tr><td>0.118</td><td>1.5</td></tr><tr><td>0.235</td><td>1.5</td></tr><tr><td rowspan="3">2.0</td><td>0.040</td><td>1.1</td><td rowspan="3">Lateral corners not rounded</td></tr><tr><td>0.167</td><td>1.1</td></tr><tr><td>0.335</td><td>1.1</td></tr></table> <p>$Re = 10^5$, Ref. 10-132.</p>	L_o/D_o	R/D_o	C_D		0.5	0.021	1.8	Fore and aft corners not rounded.	0.083	1.7	0.167	1.7	1.0	0.015	1.5		0.118	1.5	0.235	1.5	2.0	0.040	1.1	Lateral corners not rounded	0.167	1.1	0.335	1.1
L_o/D_o	R/D_o	C_D																											
0.5	0.021	1.8	Fore and aft corners not rounded.																										
	0.083	1.7																											
	0.167	1.7																											
1.0	0.015	1.5																											
	0.118	1.5																											
	0.235	1.5																											
2.0	0.040	1.1	Lateral corners not rounded																										
	0.167	1.1																											
	0.335	1.1																											
16. Rounded Nose Section 	<table><tr><th>L/D</th><th>C_D</th></tr><tr><td>0.5</td><td>1.16</td></tr><tr><td>1.0</td><td>0.90</td></tr><tr><td>2.0</td><td>0.70</td></tr><tr><td>4.0</td><td>0.68</td></tr><tr><td>6.0</td><td>0.64</td></tr></table> <p>Ref. 10-102, p. 3-12.</p>	L/D	C_D	0.5	1.16	1.0	0.90	2.0	0.70	4.0	0.68	6.0	0.64																
L/D	C_D																												
0.5	1.16																												
1.0	0.90																												
2.0	0.70																												
4.0	0.68																												
6.0	0.64																												
17. Thin Flat Plate Normal to Flow 	<p>1.9</p> <p>$Re \sim 10^5$, Ref. 10-165.</p>																												

Table 10-18. Drag of Two-Dimensional Bluff Sections. (Continued)

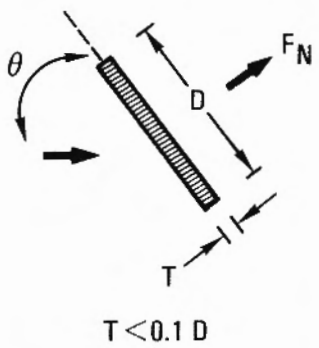
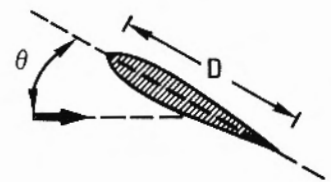
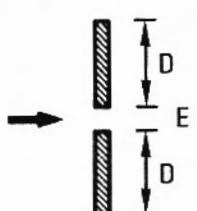
Geometry	Drag Coefficient, C_D , and Remarks																
<p>18. Thin Flat Plate Inclined to Flow</p>  <p>$T < 0.1 D$</p>	$C_N \approx \begin{cases} 2\pi \tan \theta, & \theta < 8^\circ \\ \frac{1}{0.222 + 0.283/\sin \theta}, & 90^\circ \geq \theta > 12^\circ \end{cases}$ $C_L = C_N \cos \theta$ $C_D = C_N \sin \theta$ <p>There is a discontinuity in the range $8^\circ < \theta < 12^\circ$ with $C_N \approx 0.8$ as flow separates from upper surface. See Table 10-14 for $\theta = 0^\circ$. Refs. 10-168; 10-169, p. 41; 10-224, p. 21-1.</p>																
<p>19. Thin Lifting Foil</p> 	$\left. \begin{aligned} C_D &= \text{order of } 0.01 \\ C_L &= 2\pi \sin \theta \\ C_M &= \pi/4 \sin 2\theta \end{aligned} \right\} \text{ for } \theta < 8^\circ$ <p>C_M clockwise about leading edge. $C_M \approx 0$ about point $D/4$ behind leading edge.</p> <p>Ref. 10-169, pp. 41-42. Also see Section 10.5.</p>																
<p>20. Two Thin Plates Side by Side</p> 	<table border="1" data-bbox="505 1050 813 1338"> <thead> <tr> <th>E/D</th><th>C_D</th></tr> </thead> <tbody> <tr> <td>0.5</td><td>1.42 or 2.20</td></tr> <tr> <td>1.0</td><td>1.52 or 2.13</td></tr> <tr> <td>2.0</td><td>1.9 or 2.10</td></tr> <tr> <td>3.0</td><td>2.0</td></tr> <tr> <td>5.0</td><td>1.96</td></tr> <tr> <td>10.0</td><td>1.9</td></tr> <tr> <td>15.0</td><td>1.9</td></tr> </tbody> </table> <p>} multiple values due to jet switch</p> <p>$Re = 4 \times 10^3$, Ref. 10-170.</p> <p>Drag on each plate.</p>	E/D	C_D	0.5	1.42 or 2.20	1.0	1.52 or 2.13	2.0	1.9 or 2.10	3.0	2.0	5.0	1.96	10.0	1.9	15.0	1.9
E/D	C_D																
0.5	1.42 or 2.20																
1.0	1.52 or 2.13																
2.0	1.9 or 2.10																
3.0	2.0																
5.0	1.96																
10.0	1.9																
15.0	1.9																

Table 10-18. Drag of Two-Dimensional Bluff Sections. (Continued)

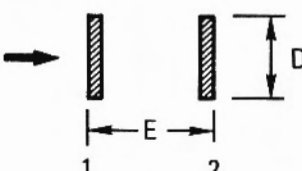
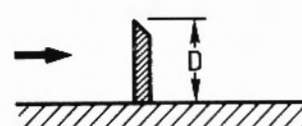
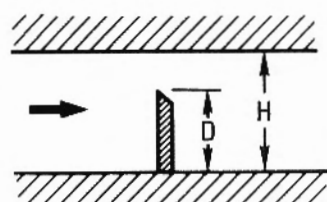
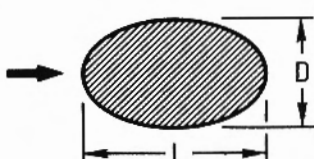
Geometry	Drag Coefficient, C_D , and Remarks																											
<p>21. Two Thin Plates in Tandem</p> 	<table><tr><th>E/D</th><th>C_{D1}</th><th>C_{D2}</th></tr><tr><td>2</td><td>1.80</td><td>0.10</td></tr><tr><td>3</td><td>1.70</td><td>0.67</td></tr><tr><td>4</td><td>1.65</td><td>0.76</td></tr><tr><td>6</td><td>1.65</td><td>0.95</td></tr><tr><td>10</td><td>1.9</td><td>1.00</td></tr><tr><td>20</td><td>1.9</td><td>1.15</td></tr><tr><td>30</td><td>1.9</td><td>1.33</td></tr><tr><td>∞</td><td>1.9</td><td>1.9</td></tr></table> <p>$Re = 4 \times 10^3$, Ref. 10-170.</p>	E/D	C_{D1}	C_{D2}	2	1.80	0.10	3	1.70	0.67	4	1.65	0.76	6	1.65	0.95	10	1.9	1.00	20	1.9	1.15	30	1.9	1.33	∞	1.9	1.9
E/D	C_{D1}	C_{D2}																										
2	1.80	0.10																										
3	1.70	0.67																										
4	1.65	0.76																										
6	1.65	0.95																										
10	1.9	1.00																										
20	1.9	1.15																										
30	1.9	1.33																										
∞	1.9	1.9																										
<p>22. Thin Plate Extending from a Wall</p> 	<p>1.4</p> <p>$Re = 5 \times 10^4$, Refs. 10-131, 10-166. See Table 10-15 for other protuberances from a surface.</p>																											
<p>23. Thin Plate Extending Part Way Across a Channel</p> 	$C_D = \frac{1.4}{(1 - D/H)^{2.85}}$ <p>for $0 < D/H < 0.25$.</p> <p>$Re > 10^3$, Ref. 10-131.</p>																											
<p>24. Ellipse</p> 	<table><tr><th>D/L</th><th>C_D</th></tr><tr><td>0.125</td><td>0.22</td></tr><tr><td>0.25</td><td>0.3</td></tr><tr><td>0.50</td><td>0.6</td></tr><tr><td>1.0</td><td>1.0</td></tr><tr><td>2.0</td><td>1.6</td></tr></table> <p>$Re = 10^5$, Refs. 10-132, 10-167.</p>	D/L	C_D	0.125	0.22	0.25	0.3	0.50	0.6	1.0	1.0	2.0	1.6															
D/L	C_D																											
0.125	0.22																											
0.25	0.3																											
0.50	0.6																											
1.0	1.0																											
2.0	1.6																											

Table 10-18. Drag of Two-Dimensional Bluff Sections. (Continued)

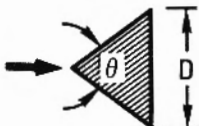
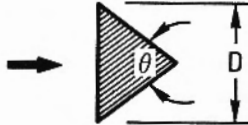
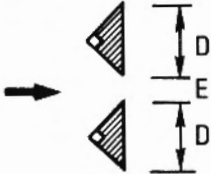
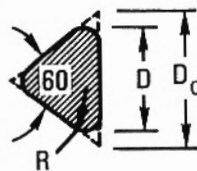
Geometry	Drag Coefficient, C_D , and Remarks																							
25. Isosceles Triangle with Point into Flow		<table><tr><th>θ (deg)</th><th>C_D</th></tr><tr><td>30</td><td>1.1</td></tr><tr><td>60</td><td>1.4</td></tr><tr><td>90</td><td>1.6</td></tr><tr><td>120</td><td>1.75</td></tr></table>	θ (deg)	C_D	30	1.1	60	1.4	90	1.6	120	1.75	$Re = 10^4$, Ref. 10-167.											
θ (deg)	C_D																							
30	1.1																							
60	1.4																							
90	1.6																							
120	1.75																							
26. Isosceles Triangle with Point Out of Flow		<table><tr><th>θ (deg)</th><th>C_D</th></tr><tr><td>30</td><td>1.9</td></tr><tr><td>60</td><td>2.1</td></tr><tr><td>90</td><td>2.15</td></tr><tr><td>120</td><td>2.05</td></tr></table>	θ (deg)	C_D	30	1.9	60	2.1	90	2.15	120	2.05	$Re = 10^4$, Ref. 10-167.											
θ (deg)	C_D																							
30	1.9																							
60	2.1																							
90	2.15																							
120	2.05																							
27. Two Isosceles Right Triangles Side by Side		<table><tr><th>E/D</th><th>C_D</th><th>C_L</th></tr><tr><td>0</td><td>1.7</td><td>0.5</td></tr><tr><td>0.25</td><td>1.2 or 0.4</td><td>0.3 or 0.4</td></tr><tr><td>0.5</td><td>1.2 or 1.8</td><td>0.2 or 0.3</td></tr><tr><td>1.0</td><td>1.1 or 1.9</td><td>0.15 or 0.25</td></tr><tr><td>2.0</td><td>1.75</td><td>0.1</td></tr><tr><td>3.0</td><td>1.75</td><td>0.08</td></tr></table>	E/D	C_D	C_L	0	1.7	0.5	0.25	1.2 or 0.4	0.3 or 0.4	0.5	1.2 or 1.8	0.2 or 0.3	1.0	1.1 or 1.9	0.15 or 0.25	2.0	1.75	0.1	3.0	1.75	0.08	<p>multiple values due to jet switch</p> <p>Lift force is repulsive.</p> <p>$Re = 2 \times 10^4$, Ref. 10-162.</p>
E/D	C_D	C_L																						
0	1.7	0.5																						
0.25	1.2 or 0.4	0.3 or 0.4																						
0.5	1.2 or 1.8	0.2 or 0.3																						
1.0	1.1 or 1.9	0.15 or 0.25																						
2.0	1.75	0.1																						
3.0	1.75	0.08																						
28. Rounded Isosceles Triangle		<table><tr><th rowspan="2">R/D</th><th colspan="2">C_D</th></tr><tr><th>\rightarrow</th><th>\leftarrow</th></tr><tr><td>0.</td><td>1.4</td><td>2.1</td></tr><tr><td>0.021</td><td>1.2</td><td>2.0</td></tr><tr><td>0.083</td><td>1.3</td><td>1.9</td></tr><tr><td>0.25</td><td>1.1</td><td>1.3</td></tr></table>	R/D	C_D		\rightarrow	\leftarrow	0.	1.4	2.1	0.021	1.2	2.0	0.083	1.3	1.9	0.25	1.1	1.3	$Re = 10^5$, Ref. 10-132.				
R/D	C_D																							
	\rightarrow	\leftarrow																						
0.	1.4	2.1																						
0.021	1.2	2.0																						
0.083	1.3	1.9																						
0.25	1.1	1.3																						

Table 10-18. Drag of Two-Dimensional Bluff Sections. (Continued)

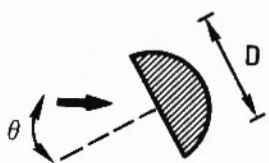

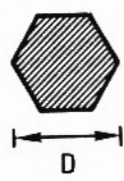
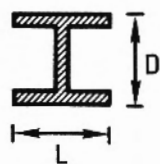
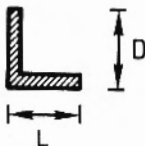
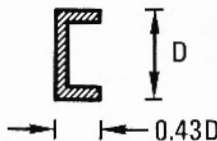
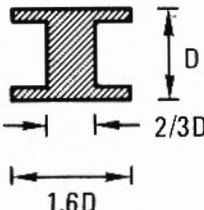
Geometry	Drag Coefficient, C_D , and Remarks																																			
29. D Section		<table><thead><tr><th>θ (deg)</th><th>C_D</th><th>C_L</th></tr></thead><tbody><tr><td>0</td><td>2.15</td><td>0</td></tr><tr><td>20</td><td>1.85</td><td>0.65</td></tr><tr><td>40</td><td>0.90</td><td>1.40</td></tr><tr><td>60</td><td>0.85</td><td>1.05</td></tr><tr><td>80</td><td>0.5</td><td>0.16</td></tr><tr><td>90</td><td>0.55</td><td>-0.30</td></tr><tr><td>120</td><td>0.90</td><td>-0.05</td></tr><tr><td>140</td><td>1.15</td><td>0.03</td></tr><tr><td>160</td><td>1.20</td><td>0.01</td></tr><tr><td>180</td><td>1.15</td><td>0</td></tr></tbody></table>	θ (deg)	C_D	C_L	0	2.15	0	20	1.85	0.65	40	0.90	1.40	60	0.85	1.05	80	0.5	0.16	90	0.55	-0.30	120	0.90	-0.05	140	1.15	0.03	160	1.20	0.01	180	1.15	0	
θ (deg)	C_D	C_L																																		
0	2.15	0																																		
20	1.85	0.65																																		
40	0.90	1.40																																		
60	0.85	1.05																																		
80	0.5	0.16																																		
90	0.55	-0.30																																		
120	0.90	-0.05																																		
140	1.15	0.03																																		
160	1.20	0.01																																		
180	1.15	0																																		
Ref. 10-171.																																				
30. Cup Section		$\rightarrow C_D = 2.3$ $\leftarrow C_D = 1.1$ $Re = 2 \times 10^4$, Ref. 10-167.																																		
31. Hexagon		$\rightarrow C_D = 1.0$ $\uparrow C_D = 0.7$ Ref. 10-161.																																		
32. I Shape		<table><thead><tr><th rowspan="3">Flow Direction</th><th colspan="2">C_D</th></tr><tr><th colspan="2">L/D</th></tr><tr><th>0.5</th><th>1.0</th></tr></thead><tbody><tr><td>\rightarrow</td><td>2.05</td><td>1.6</td></tr><tr><td>\uparrow</td><td>0.9</td><td>1.9</td></tr></tbody></table>	Flow Direction	C_D		L/D		0.5	1.0	\rightarrow	2.05	1.6	\uparrow	0.9	1.9																					
Flow Direction	C_D																																			
	L/D																																			
	0.5	1.0																																		
\rightarrow	2.05	1.6																																		
\uparrow	0.9	1.9																																		

Table 10-18. Drag of Two-Dimensional Bluff Sections. (Continued)

Geometry	Drag Coefficient, C_D , and Remarks																																														
<p>33. L Shape</p> 	<table><tr><th rowspan="3">Flow Direction</th><th colspan="2">C_D</th><th colspan="2">C_L</th></tr><tr><th colspan="2">L/D</th><th colspan="2">L/D</th></tr><tr><th>0.5</th><th>1.0</th><th>0.5</th><th>1.0</th></tr><tr><td>→</td><td>2.0</td><td>2.0</td><td>-0.1</td><td>-0.3</td></tr><tr><td>↗</td><td>--</td><td>2.0</td><td>--</td><td>0</td></tr><tr><td>↑</td><td>--</td><td>2.0</td><td>--</td><td>0.3</td></tr><tr><td>←</td><td>1.9</td><td>1.8</td><td>0.95</td><td>2.1</td></tr><tr><td>↖</td><td>1.8</td><td>2.5</td><td>-0.7</td><td>0</td></tr><tr><td>↓</td><td>1.7</td><td>1.8</td><td>-1.7</td><td>-2.1</td></tr></table> <p>Ref. 10-172.</p>				Flow Direction	C_D		C_L		L/D		L/D		0.5	1.0	0.5	1.0	→	2.0	2.0	-0.1	-0.3	↗	--	2.0	--	0	↑	--	2.0	--	0.3	←	1.9	1.8	0.95	2.1	↖	1.8	2.5	-0.7	0	↓	1.7	1.8	-1.7	-2.1
Flow Direction	C_D		C_L																																												
	L/D		L/D																																												
	0.5	1.0	0.5	1.0																																											
→	2.0	2.0	-0.1	-0.3																																											
↗	--	2.0	--	0																																											
↑	--	2.0	--	0.3																																											
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↓	1.7	1.8	-1.7	-2.1																																											
<p>34. Channel Section</p> 	<p>→ 1.8 ← 2.05 ↑ 0.6</p> <p>Ref. 10-172.</p>																																														
<p>35. Built-Up Section</p> 	<p>→ 1.4 ↑ 2.2</p> <p>Ref. 10-172.</p>																																														